

YOUR REF 來函檔號:

OUR REF 本署檔號: FAX 圖文傳真:

2523 9380

TEL 電話: WEBSITE 網址:

3842 3507 www.bd.gov.hk

(17) in BD GR/1-50/76(VII)

23 February 2022

To: All

Authorized Persons

Registered Structural Engineers Registered Geotechnical Engineers

Registered Inspectors

Registered General Building Contractors

Registered Specialist Contractors Registered Minor Works Contractors

Dear Sir/Madam,

#### Amendments to Code of Practice for Structural Use of Concrete 2013 (2020 Edition)

The Technical Committee (TC) on the Code of Practice for Structural Use of Concrete 2013 (the Code) set up by the Buildings Department (BD) regularly collects views and feedback from the practitioners and the stakeholders arising from the use of the Code, and reviews the contents thereof for recommending the necessary update.

- 2. Having considered the TC's recommendations, certain amendments to the Code (as detailed at the Appendix) are promulgated with immediate effect from the date of this letter. The amendments have been uploaded to BD website www.bd.gov.hk under the "Codes, design manuals and guidelines" page of the "Resources" section.
- 3. The amendments to the Code include:
  - (a) clause 6.2.3 and Figure 6.18b addition of design requirements for plain concrete linings;
  - (b) clause 10.3.4.2 and Table 10.2 revision of the requirements on the use of 100 mm and 150 mm concrete cubes;

/(c) ...

- clause 11.7.5.4 and Table 11.2 addition of general guidelines on (c) monitoring early compressive strength of insitu concrete by maturity method; and
- Annex A addition of ASTM C1074-19 $^{\epsilon 1}$  corresponding to the new (d) clause 11.7.5.4.

Yours faithfully,

( AU YEUNG Hoi-pang ) Assistant Director New Buildings 2 for Building Authority

# Amendments to the Code of Practice for Structural Use of Concrete 2013 (2020 Edition) (February 2022)

#### Legends:



**Amendments to the Code of Practice for Structural Use of Concrete 2013 (2020 Edition)** 

Item	Amendments to the Code of Practice for Structure  Current version	Amendments
Ittiii		
1. Contents	6.2.2 Walls	6.2.2 Walls 6.2.3 Plain concrete linings
2. LIST OF TABLES <sup>1</sup>	Table 11.1 – Objects of production and construction control Table 12.1 – Design flexural tensile stresses for class 2 members: serviceability limit state: cracking	Table 11.1 – Objects of production and construction control  Table 11.2 – Correction factor applied to the estimated insitu  concrete compressive strength  Table 12.1 – Design flexural tensile stresses for class 2 members:  serviceability limit state: cracking
3. LIST OF FIGURES <sup>2</sup>	Figure 6.18a - Geometry of the Circular Section Figure 6.19 - Critical section for shear check in a pile cap	Figure 6.18a - Geometry of the Circular Section  Figure 6.18b - Interaction Curve for Design of Plain Concrete  Lining  Figure 6.19 - Critical section for shear check in a pile cap
4. Clause 6.2.3 and Figure 6.18b		<ul> <li>6.2.3 Plain concrete linings</li> <li>6.2.3.1 General</li> <li>Plain concrete is suitable for use in structural members with high axial loads and relatively low bending moments. The following criteria can generally be applied to the use of plain concrete lining in tunnels or caverns: <ul> <li>(a) the lining curvature is adequate to accommodate axial distribution of external loads;</li> <li>(b) the plain concrete lining is constructed in relatively good rock geology and is always in compression under all load combinations;</li> <li>(c) the effect of imperfection of the concrete lining has been considered by means of rigorous structural analysis of the plain concrete lining; and</li> </ul> </li> </ul>

<sup>&</sup>lt;sup>1</sup> Addition of Table 11.2 corresponding to the new clause 11.7.5.4.

<sup>&</sup>lt;sup>2</sup> Addition of Figure 6.18b corresponding to the new clause 6.2.3.

Item	Current version	Amendments
		<ul> <li>(d) an arch section can be formed by plain concrete in conjunction with a reinforced concrete invert provided the junction between the plain and reinforced concrete satisfies the design requirements specified in clause 6.2.3.2.</li> <li>6.2.3.2 Design of plain concrete lining  (a) Maximum axial load for plain concrete lining</li> </ul>
		The design ultimate capacity of axial load per unit length, $n_{LT}$ and design maximum ultimate bending moment per unit length, $m_{LT}$ (= $n_{LT}$ $e_{\chi}$ ) shall be evaluated using the interaction curve as shown in Figure 6.18b.
		(i) The first section (Point 1 to Point 2) of the interaction curve as shown in Figure 6.18b, the highest axial force, is applicable when the eccentricity of the thrust force is less than or equal to 0.1h. The ultimate capacity is calculated using a rectangular stress block over the whole section;  For $e_X \le 0.1$ h $n_{LT} \le 0.32$ h $f_{cu}$ 6.63a
		(ii) The second section (Point 2 to Point 3) of the interaction diagram is based on a rectangular stress block approach and is applicable for eccentricity between 0.1h and 0.3h. The stress block is acting over part of the section, and reduces as the eccentricity increases.  For $0.1h < e_x \le 0.3h$ $n_{LT} \le 0.4 (h-2 e_x) f_{cu}$ 6.63b
		where:

Item	Current version	Amendments			
		$e_{\chi}$ is the resultant eccentricity of load at right			
		angles to the plan of the lining.			
		(iii) Cracking restriction limits the use of the strength design method to a maximum eccentricity of 0.3h. The third section (Point 3 to Point 4) of the interaction curve is a straight line down to the point $n_{LT} = 0$ , as shown in Figure 6.18b.			
		Point 1 Point 2			
		ε ·			
		Axial Load, n <sub>LT</sub> (kN/m)  Boint 3			
l		Axial Loa			
		Point 4 Bending Moment, $m_{LT}$ (kNm/m)			
		Figure 6.18b – Interaction Curve for Design of Plain Concrete Lining			

Item	Current version							Amendments			
							(b) Shear strength  The design shear stress in the plain concrete lining subjected to shear and axial compression without shear reinforcement can be calculated in accordance with clause 6.1.2.5(k).  The design shear resistance of plain concrete lining can be checked in accordance with clause 6.2.2.3(r).				
5. Clause 10.3.4.2(a)	10.3.4.2 Concrete Cube Tests During Construction					1			Tests During Constru	ction	
6. Table 10.2	(a) Concrete Cubes  The compressive strength of concrete shall be determined by testing 100 mm or 150 mm cubes 28 days after mixing.  A representative sample shall be taken from fresh concrete to make test cubes and each sample shall be taken from a single batch. The rate of sampling shall be at least that specified in Table 10.1 and at least one sample shall be taken from each grade of concrete produced on any one day.					ter mixing. sh concrete ken from a t least that le shall be	(a) Concrete Cubes  The compressive strength of concrete shall be determined by testing 100 mm cubes, or 150 mm cubes if the maximum aggregate size of concrete exceeds 20 mm, 28 days after mixing.  A representative sample shall be taken from fresh concrete to make test cubes and each sample shall be taken from a single batch. The rate of sampling shall be at least that specified in Table 10.1 and at least one sample shall be taken from each grade of concrete produced on any one day.				
	Specified	Compliance	Colu	mn A	Coli	umn B	Specified	Compliance	Column A	Column B	
	Grade Strength	Criteria			Grade Strength	Criteria	Average of 4 consecutive test results shall exceed the specified grade strength by at least	Any individual test result shall not be less than the specified grade strength minus			
			150 mm Cubes	100 mm Cubes	150 mm Cubes	100 mm Cubes			100 mm Cubes (150 mm Cubes)	100 mm Cubes (150 mm Cubes )	
	C20 and	C1	5 MPa	7 MPa	3 MPa	2 MPa	C20 and above	C1	7 MPa (5 MPa)	2 MPa (3 MPa)	
	above	C2	3 MPa	5 MPa	3 MPa	2 MPa		C2	5 MPa	2 MPa	
	Below	C1 or C2	2 MPa	3 MPa	2 MPa	2 MPa			(3 MPa)	(3 MPa)	

Item	Current version	Amendments			
	Table 10.2 - Compressive Strength Compliance Criteria	Below C1 or C2 3 MPa 2 MPa (2 MPa)  Table 10.2 - Compressive Strength Compliance Criteria			
7. Clause 10.3.4.2(b) (i)	(i) Before 40 test results are available, where there is sufficient previous production data using similar materials from the same plant under similar supervision to establish that the standard deviation of 40 test results is less than 5 MPa for 150 mm test cubes or 5.5 MPa for 100 mm test cubes, compliance requirement C2 may be adopted; otherwise compliance requirement C1 shall be adopted.	(i) Before 40 test results are available, where there is sufficient previous production data using similar materials from the same plant under similar supervision to establish that the standard deviation of 40 test results is less than 5.5 MPa (5 MPa for 150 mm cubes), compliance requirement C2 may be adopted; otherwise compliance requirement C1 shall be adopted.			
8. Clause 10.3.4.2(b) (ii)	(ii) Where the calculated standard deviation of a set of 40 consecutive test results of concrete judged by compliance requirement C2 of Table 10.2 exceeds 5 MPa for 150 mm test cubes or 5.5 MPa for 100 mm test cubes, compliance requirement for checking the test results shall be changed from C2 to C1 on the 35 <sup>th</sup> day after making the last pair of test cubes in the set of 40.	(ii) Where the calculated standard deviation of a set of 40 consecutive test results of concrete judged by compliance requirement C2 of Table 10.2 exceeds 5.5 MPa (5 MPa for 150 mm cubes), compliance requirement for checking the test results shall be changed from C2 to C1 on the 35 <sup>th</sup> day after making the last pair of test cubes in the set of 40.			
9. Clause 10.3.4.2(b) (iii)	(iii) Where the calculated standard deviation of 40 previous consecutive test results is less than 5 MPa for 150 mm test cubes or 5.5 MPa for 100 mm test cubes, compliance requirement shall be changed from C1 to C2 on the 35 <sup>th</sup> day after making the last pair of test cubes in the set of 40.	(iii) Where the calculated standard deviation of 40 previous consecutive test results is less than 5.5 MPa (5 MPa for 150 mm cubes), compliance requirement shall be changed from C1 to C2 on the 35th day after making the last pair of test cubes in the set of 40.			

Item	Current version	Amendments
10. Clause 10.3.4.2(b) (iv)	(iv) For concrete grade not exceeding C60, the calculated standard deviation exceeds 8 MPa for 150 mm test cubes or 8.5 MPa for 100 mm test cubes; or	(iv) For concrete grade not exceeding C60, the calculated standard deviation exceeds 8.5 MPa (8 MPa for 150 mm cubes); or
11. Clause 10.3.4.2(b) (vi)	(vi) The average of the latest 40 cube test results exceeds the grade strength by at least 10 MPa for 150 mm test cubes or 12 MPa for 100 mm test cubes and all individual test results exceeds the grade strength by at least 4 MPa for 150 mm test cubes or 5 MPa for 100 mm test cubes; or	(vi) The average of the latest 40 cube test results exceeds the grade strength by at least 12 MPa (10 MPa for 150 mm cubes) and all individual test results exceeds the grade strength by at least 5 MPa (4 MPa for 150 mm cubes); or
12. Clause 11.7.5.4 and Table 11.2		11.7.5.4 Monitoring early compressive strength of insitu concrete by maturity method  After concrete casting, the development of insitu concrete compressive strength at early age can be monitored by the maturity method. The maturity method can be used for estimating insitu concrete compressive strength through measurement of the temperature-time history of concrete of ages up to 14 days after casting, for the purpose of determining the concrete strength for striking of formwork and falsework¹ in lieu of the minimum periods specified in clause 10.3.8.2. In formulating a proposal adopting the maturity method, reference should be made to the acceptable standard in Annex A. The proposal should cover the following:  (a) choice of an appropriate maturity function and determination of maturity function constants;  (b) apparatuses and their calibration;  (c) procedure for developing strength-maturity relationship;  (d) procedure for estimating insitu concrete strength;  (e) validation of insitu concrete strength;

	(f) re-calibration and re-validation; and			
	(g) quality assurance and supervision.			
	The concrete mix used in the structure should be the same as that used to derive the strength-maturity relationship.			
	Taking into account the different conditions between cast insitu concrete and concrete cubes under various curing temperatures in the calibration process, a correction factor as shown in Table 11.2 should be applied to the estimated insitu concrete compressive strength.			
	Type of concrete mix  Solution			
	Concrete mix containing pfa or ggbs 0.7 0.8			
	Other concrete mix 0.8			
	Table 11.2 – Correction factor applied to the estimated insitu concrete compressive strength			
	1 Due to the rapid rate of concrete strength development within 24 hours after concrete casting, the maturity method is not suitable for use in justifying minimum periods before striking formwork and falsework of less than 24 hours.			

Item	Cu	rrent version	Amendments		
13. Annex A <sup>3</sup>	+A1:2009	Silica fume for concrete.  Definitions, requirements and conformity criteria	BS EN 13263-1:2005 +A1:2009 ASTM C1074-19 <sup>e1</sup>	Silica fume for concrete. Definitions, requirements and conformity criteria  Standard Practice for Estimating Concrete Strength by the Maturity Method	

.

<sup>&</sup>lt;sup>3</sup> Addition of ASTM C1074-19<sup>ε</sup>1 corresponding to the new clause 11.7.5.4.