

Amendments to the Code of Practice for Foundations 2017 (2024 Edition)
(September 2025)

Legends:

 New/Amended

 Deleted

(9/2025)

Amendments to the Code of Practice for Foundations 2017 (2024 Edition)

Item	Current version	2025 Amendments
1. Clause 2.2.4 ¹	<p>Allowable Vertical Bearing Pressure of Shallow Foundation founded on Soil</p> <p>The allowable vertical bearing pressure of foundations founded on soils derived by bearing capacity equation may be taken as:</p> $q_a = \frac{q_u - q_o}{F} + q_o$ <p>where q_a = allowable vertical bearing pressure q_u = ultimate bearing capacity of the granular soil, which should be limited to 3 000 kPa</p> <p>q_o = effective overburden pressure at the base of the foundation, i.e. $q_o = \gamma_s' D_f$, where γ_s' and D_f are respectively the effective unit weight and depth of the soil that originally exists above the base of the foundation</p> <p>F = factor of safety not less than 3</p>	<p>Allowable Vertical Bearing Pressure of ↓ Foundation Founded on Soil</p> <p>The allowable vertical bearing pressure of foundations founded on soils derived by bearing capacity equation may be taken as:</p> $q_a = \frac{q_u - q_o}{F} + q_o$ <p>where q_a = allowable vertical bearing pressure q_u = ultimate bearing capacity of the granular soil, which should be limited to 3 000 kPa. For foundations supporting building(s) with basement(s) on granular soil, this limit should be increased to 4 500 kPa.</p> <p>q_o = effective overburden pressure at the base of the foundation, i.e. $q_o = \gamma_s' D_f$, where γ_s' and D_f are respectively the effective unit weight and depth of the soil that originally exists above the base of the foundation</p> <p>F = factor of safety not less than 3</p>

¹ Revision of the maximum value of ultimate bearing capacity.

Item	Current version	2025 Amendments
2. Clause 2.2.4 Note 1 ²	<p>Notes:</p> <p>(1) q should not include any overburden pressure that may be temporarily or permanently removed during the design life of the foundation. In its derivation, the maximum effective overburden depth of subsoil should not be greater than 3 m or B_f, whichever is the lesser, and suitable adjustments should be made to discount any voids that may be allowed for underground utilities.</p>	<p>Notes:</p> <p>(1) q should not include any overburden pressure that may be temporarily or permanently removed during the design life of the foundation. ↓ In the derivation of q for shallow foundation, the depth of subsoil should not exceed 3 m or B_f, whichever is the smaller. For foundations supporting building(s) with basement(s) on granular soil, the effective depth of subsoil, defined as the minimum overburden depth around the basement perimeter, should not exceed 10 m or B_f, whichever is the smaller, in the derivation of q. Suitable adjustments should be made to discount any voids that may be allowed for underground utilities.</p>

² Revision of the maximum effective overburden depth of subsoil.

Item	Current version	2025 Amendments
3. Clause 2.3.1(4) paragraph 2 ³	<p>(4) Young's Modulus ...</p> <p>Care should be taken in determining the Young's modulus of soils by the use of empirical correlations with the SPT N-value as it can be unsafe in some cases and over-conservative in others. For shallow foundations with design allowable bearing pressures not greater than 250 kPa, in the absence of more accurate data, the Young's modulus E_s (in MPa) of granular soils may be taken as one time the SPT N-value.</p>	<p>(4) Young's Modulus ...</p> <p>Care should be taken in determining the Young's modulus of soils by the use of empirical correlations with the SPT N-value as it can be unsafe in some cases and over-conservative in others. For shallow foundations ↓, in the absence of more accurate data, the Young's modulus E_s (in MPa) of granular soils may be taken as ↓ 1 times the SPT N-value. For raft foundation on granular soils derived from in-situ rock weathering (e.g. saprolites and residual soils) with SPT N-value > 30, in the absence of more accurate data, the Young's modulus E_s (in MPa) may be taken as 1.5 times the SPT N-value.</p>

³ Revision of the requirement for determination of Young's modulus.

Item	Current version	2025 Amendments
4. Clause 4.2.2(2)(c) ⁴	<p>(2) Testing Requirements</p> <p>...</p> <p>(c) the Young's modulus, E_s (in MPa), of the bearing strata used in the estimation of settlement is greater than one time the SPT N-value.</p>	<p>(2) Testing Requirements</p> <p>...</p> <p>(c) the Young's modulus, E_s (in MPa), of the bearing strata used in the estimation of settlement is greater than ↓ 1 times the SPT-N value or 1.5 times the SPT N-value (for granular soils derived from in-situ rock weathering (e.g. saprolites and residual soils) with SPT N-value > 30) as appropriate.</p>
5. Table 7.2	<p>Table 7.2 Typical Values for the Three Triggering Levels on Nearby Buildings, Structures or Services that are not Sensitive to Settlement</p> <p>...</p>	<p>Table 7.2 Typical Values for the Three Triggering Levels on Nearby Buildings, Structures, Land or Services that are not Sensitive to Settlement</p> <p>...</p>

⁴ Revision of the requirement for plate load test.

Item	Current version	2025 Amendments
6. Clause 8.10 paragraph 4 ⁵	<p>TENSION LOADING TEST</p> <p>...</p> <p>The maximum test load should not result in the test pile or anchor being stressed beyond the yield stress. Where the design uplift capacity of the test pile is based on bond and tensile stresses which are taken as 50% of the corresponding values in compression, the test load may be 1.5 times the design uplift capacity of the pile under working load.</p>	<p>TENSION LOADING TEST</p> <p>...</p> <p>The maximum test load should not result in the test pile or anchor being stressed beyond the yield stress. Where the design ↓ tension capacity of test pile is based on bond ↓ or friction between rock/soil and concrete/grout for pile and is taken as not exceeding 50% of the corresponding ↓ allowable bond stress in compression, the test load may be set at 1.5 times the design ↓ tension capacity ↓.</p>

⁵ Refinement of the wording.