Amendments to the Code of Practice for Structural Use of Concrete 2013 (2020 Edition) (February 2022)

Legends:



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4. Clause 6.2.3 and Figure 6.18b		 6.2.3 Plain concrete linings 6.2.3.1 General Plain concrete is suitable for use in structural members with high axial loads and relatively low bending moments. The following criteria can generally be applied to the use of plain concrete lining in tunnels or caverns: (a) the lining curvature is adequate to accommodate axial distribution of external loads; (b) the plain concrete lining is constructed in relatively good rock geology and is always in compression under all load combinations; (c) the effect of imperfection of the concrete lining has been considered by means of rigorous structural analysis of the plain concrete lining; and

¹ Addition of Table 11.2 corresponding to the new clause 11.7.5.4.

² Addition of Figure 6.18b corresponding to the new clause 6.2.3.

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		 (d) an arch section can be formed by plain concrete in conjunction with a reinforced concrete invert provided the junction between the plain and reinforced concrete satisfies the design requirements specified in clause 6.2.3.2. 6.2.3.2 Design of plain concrete lining (a) Maximum axial load for plain concrete lining
		The design ultimate capacity of axial load per unit length, n_{LT} and design maximum ultimate bending moment per unit length, m_{LT} (= n_{LT} e_{χ}) shall be evaluated using the interaction curve as shown in Figure 6.18b.
		(i) The first section (Point 1 to Point 2) of the interaction curve as shown in Figure 6.18b, the highest axial force, is applicable when the eccentricity of the thrust force is less than or equal to 0.1h. The ultimate capacity is calculated using a rectangular stress block over the whole section; For $e_X \le 0.1$ h $n_{LT} \le 0.32$ h f_{cu} 6.63a
		(ii) The second section (Point 2 to Point 3) of the interaction diagram is based on a rectangular stress block approach and is applicable for eccentricity between 0.1h and 0.3h. The stress block is acting over part of the section, and reduces as the eccentricity increases. For $0.1h < e_x \le 0.3h$ $n_{LT} \le 0.4 (h-2 e_x) f_{cu}$ 6.63b
		where:

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		e_{χ} is the resultant eccentricity of load at right			
		angles to the plan of the lining.			
		(iii) Cracking restriction limits the use of the streedesign method to a maximum eccentricity of 0. The third section (Point 3 to Point 4) of the interaction curve is a straight line down to the point $n_{LT} = 0$, as shown in Figure 6.18b.			
		Point 1 Point 2			
		ε ·			
		Axial Load, n _{LT} (kN/m) Boint 3			
l		Axial Loa			
		Point 4 Bending Moment, m_{LT} (kNm/m)			
		Figure 6.18b – Interaction Curve for Design of Plain Concrete Lining			

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							(b) Shear strength The design shear stress in the plain concrete lining subjected to shear and axial compression without shear reinforcement can be calculated in accordance with clause 6.1.2.5(k). The design shear resistance of plain concrete lining can be checked in accordance with clause 6.2.2.3(r).				
5. Clause 10.3.4.2(a)	10.3.4.2 Concrete Cube Tests During Construction						10.3.4.2 C		Tests During Constru	ction	
6. Table 10.2	(a) Concrete Cubes The compressive strength of concrete shall be determined by testing 100 mm or 150 mm cubes 28 days after mixing. A representative sample shall be taken from fresh concrete to make test cubes and each sample shall be taken from a single batch. The rate of sampling shall be at least that specified in Table 10.1 and at least one sample shall be taken from each grade of concrete produced on any one day.					ter mixing. sh concrete ken from a t least that le shall be	The contesting aggreg A reprimake to batch.	ompressive standard at size of concesentative sandard cubes and The rate of 10.1 and at 10.0 mm.	rength of concrete shaubes, or 150 mm cubocrete exceeds 20 mm, mple shall be taken from the sampling shall be at least one sample shall oduced on any one day	28 days after mixing. om fresh concrete to taken from a single east that specified in be taken from each	
	Specified	Compliance	Colu	mn A	Coli	umn B	Specified	Compliance	Column A	Column B	
	Grade Strength Criteria Average of 4 consecutive test results shall exceed the specified grade strength by at least Criteria Any individual test result shall not be less than the specified grade strength by at least				Grade Strength	Criteria	Average of 4 consecutive test results shall exceed the specified grade strength by at least	Any individual test result shall not be less than the specified grade strength minus			
			150 mm Cubes	100 mm Cubes	150 mm Cubes	100 mm Cubes			100 mm Cubes (150 mm Cubes)	100 mm Cubes (150 mm Cubes)	
	C20 and	C1	5 MPa	7 MPa	3 MPa	2 MPa	C20 and above	C1	7 MPa (5 MPa)	2 MPa (3 MPa)	
	above	C2	3 MPa	5 MPa	3 MPa	2 MPa		C2	5 MPa	2 MPa	
	Below	C1 or C2	2 MPa	3 MPa	2 MPa	2 MPa			(3 MPa)	(3 MPa)	

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	Table 10.2 - Compressive Str	rength Compliance Cr	riteria	Below C1 or C2 3 MPa (2 MPa) Table 10.2 - Compressive Strength Compliance Criteria				
7. Clause 10.3.4.2(b) (i)	(i) Before 40 test results sufficient previous promaterials from the same to establish that the stand is less than 5 MPa for 15 100 mm test cubes, comadopted; otherwise comadopted.	plant under similar s dard deviation of 40 50 mm test cubes or 5 upliance requirement 6	similar supervision test results .5 MPa for C2 may be	pre plan dev 150	vious productiont under simila viation of 40 tes more more more more more more more more	ults are available, whom data using similar may resupervision to estable results is less than pompliance requirement call shapped to the substitute of the s	aterials from the same lish that the standard 5.5 MPa (5 MPa for t C2 may be adopted;	
8. Clause 10.3.4.2(b) (ii)	(ii) Where the calculated st consecutive test results or requirement C2 of Ta 150 mm test cubes or 5 compliance requirement shall be changed from making the last pair of to	f concrete judged by cable 10.2 exceeds 5 .5 MPa for 100 mm t for checking the t C2 to C1 on the 35th	ompliance MPa for test cubes, test results day after	con requestions from the contract of the contr	secutive test r uirement C2 of mm cubes), co ults shall be ch	ated standard deviates esults of concrete just Table 10.2 exceeds managed from C2 to C1 ir of test cubes in the second control of test cubes cubes in the second control of test cubes cubes cubes cubes cubes cubes cube cubes cube	dged by compliance 5.5 MPa (5 MPa for a for checking the test on the 35 th day after	
9. Clause 10.3.4.2(b) (iii)	(iii) Where the calculated st consecutive test results test cubes or 5.5 MPa for requirement shall be chaday after making the last 40.	is less than 5 MPa for 100 mm test cubes, conged from C1 to C2	or 150 mm compliance on the 35 th	con mm to (secutive test re <mark>cubes)</mark> , compli	lated standard deviat sults is less than 5.5 I iance requirement shal ay after making the las	MPa (5 MPa for 150 l be changed from C1	

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10. Clause 10.3.4.2(b) (iv)	(iv) For concrete grade not exceeding C60, the calculated standard deviation exceeds 8 MPa for 150 mm test cubes or 8.5 MPa for 100 mm test cubes; or	(iv) For concrete grade not exceeding C60, the calculated standard deviation exceeds 8.5 MPa (8 MPa for 150 mm cubes); or
11. Clause 10.3.4.2(b) (vi)	(vi) The average of the latest 40 cube test results exceeds the grade strength by at least 10 MPa for 150 mm test cubes or 12 MPa for 100 mm test cubes and all individual test results exceeds the grade strength by at least 4 MPa for 150 mm test cubes or 5 MPa for 100 mm test cubes; or	(vi) The average of the latest 40 cube test results exceeds the grade strength by at least 12 MPa (10 MPa for 150 mm cubes) and all individual test results exceeds the grade strength by at least 5 MPa (4 MPa for 150 mm cubes); or
12. Clause 11.7.5.4 and Table 11.2		11.7.5.4 Monitoring early compressive strength of insitu concrete by maturity method After concrete casting, the development of insitu concrete compressive strength at early age can be monitored by the maturity method. The maturity method can be used for estimating insitu concrete compressive strength through measurement of the temperature-time history of concrete of ages up to 14 days after casting, for the purpose of determining the concrete strength for striking of formwork and falsework¹ in lieu of the minimum periods specified in clause 10.3.8.2. In formulating a proposal adopting the maturity method, reference should be made to the acceptable standard in Annex A. The proposal should cover the following: (a) choice of an appropriate maturity function and determination of maturity function constants; (b) apparatuses and their calibration; (c) procedure for developing strength-maturity relationship; (d) procedure for estimating insitu concrete strength; (e) validation of insitu concrete strength;

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		(f) re-calibration and re-validation; and			
		(g) quality assurance and supervision.			
		The concrete mix used in the structure should be the same as that used to derive the strength-maturity relationship.			
		Taking into account the di concrete and concrete cubes the calibration process, a coshould be applied to the estrength.	s under various cur rrection factor as s	ing temperatures in hown in Table 11.2	
		Type of concrete mix	≤ 48 hours after concrete casting	> 48 hours after concrete casting	
		Concrete mix containing pfa or ggbs	0.7	0.8	
		Other concrete mix	0.8	0.8	
		Table 11.2 – Correction faconcrete compressive stren		ne estimated insitu	
		1 Due to the rapid rate of concrete s casting, the maturity method is not su striking formwork and falsework of lo	itable for use in justifyin		

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13. Annex A ³	+A1:2009	Silica fume for concrete. Definitions, requirements and conformity criteria	BS EN 13263-1:2005 +A1:2009 ASTM C1074-19 ^{e1}	Silica fume for concrete. Definitions, requirements and conformity criteria Standard Practice for Estimating Concrete Strength by the Maturity Method	

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³ Addition of ASTM C1074-19^ε1 corresponding to the new clause 11.7.5.4.